REPORT ON

SOIL INVESTIGATION FOR CONSTRUCTION OF + 2 SCHOOL AT UPGRADED UCCCH MAADHYAMIK VIDYALAY,GANNIPUR,SAKRAICHA,PHULWARI SHARIF,PATNA

Submitted to

MANAGING DIRECTOR
BSEIDC, PATNA.

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PREFACE

The present report on sub-soil investigation was carried out as per Managing Director, BSEIDC, Patna letter no BSEIDC/TECH/1960/2018-1368 dated 02.03.2021 .

The entire investigation process was broadly divided into two category –one field work and second was laboratory work.

Field work includes conducting SPT ,Dynamic cone test, collection of disturbed as well as undisturbed soil samples from different location and different depth of sub-soil strata.

It was tried to get information from local people to get an idea about variation of water table during different season of year and also to get first hand information about type of foundation usually provided in the locality.

We thanks Prof. M.P.Jakhanwal ,M.Tech ,Ph.D. ,Muzaffarpur Institute of Technology, Muzaffarpur for his valuable advice during laboratory test and during preparation of report.

Client's help is gratefully acknowledged in providing Bore hole locations, cooperation and guidance during finalization of report.

We belief that the present report will serve the purpose, for which sub-soil investigation has been carried out.

Subodh Kumar Sinha

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Partner, Shamvwi Consultant

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REPORT ON SUB-SOIL INVESTIGATION FOR THE CONSTRUCTION OF + 2 SCHOOL AT UPGRADED UCCCH MAADHYAMIK VIDYALAY, GANNIPUR, SAKRAICHA, PHULWARI SHARIF,PATNA.

1. INTRODUCTION

The objective of subsoil investigation reported here in, were taken up, to find out the nature of subsoil at the site of the proposed construction and to recommend the type or types of foundation suitable for it and the corresponding allowable bearing capacity.

The necessary field tests were carried out at the site. Soil samples from various depths in the different bore holes were collected, transported, carefully to the laboratory and tested to determine the engineering properties of the soil.

Based on the test results, certain recommendation were made and given in this report, regarding the type of foundation suitable for the proposed project and the allowable bearing capacity for certain sizes thereof.

2. TOPOGRAPHY

The land in question was even.

3. FIELD WORK

The field work consists of boring, soil sampling and conduct of Standard penetration tests and Dynamic cone penetration tests.

3.1 BORING

An appropriate number of boreholes of adequate depth were sunk at suitable spots as per direction of Engineer-in-charge. The details of the boreholes are given in table-1.

Table 1: Details of bore holes

DIAMETER OF BORE MM	DEPTH M	BORE HOLE
150	10.5	3 Bore Holes (BH-1 to BH-3)

The borings were kept dry while advancing through partially saturated soil. The position of water table in a borehole was recorded at least 48 hours after the stopping of the boring operation.

For boring below ground water level, the borehole was kept filled with water upto that level during boring.

3.2 SAMPLING

Undisturbed & disturbed samples were collected at different depth/where change of strata occurred. Identification slips were provided both inside and outside the tube.
On arrival in laboratory, the identification slips were checked against the boring and sampling records.
Samples were extracted from the tubes just before testing.

3.3 STANDARD PENETRATION TEST

This test was performed in the boreholes at interval of depth of 1.5m, or at the change of starta/ as per IS: 2131 of 1963.

3.4 DYNAMIC CONE PENETRATION TEST

This test was performed when a bore hole could not be advanced to desired depth due to caving- in of the soil, or when it was felt necessary to supplement the information gained from SPT. This test was performed, as per

relevant IS code till high value of penetration resistance was encountered or till desired depth of investigation was reached, at which stage the test was stopped.

4. LABORATORY TEST

Lab. Test was performed to determine the following properties of soil samples as per relevant I.S. code.
(a) Natural moisture content.
(b)Bulk density.
(c) Atterberg' s limits (on fine grained soil only)
(d) Grain size analysis.
(e) Specific gravity.
(f) Shear test.
(i) Unconfined/triaxial compression tests for fine-grained soils.
(ii) Direct shear test for coarse-grained soils.
(g)Consolidation tests for fine grained soils.
(h) Organic content, chemical test etc.
(i) pH of soil and water.
(j) Free swell Index
(k)Crushing strength test (uniaxial)

4.1 SAMPLE EXTRACTION & PREPARATION OF TEST SPECIMENS

Samples for different tests were prepared as per method described in relevant IS code/as per method described in standard book.

4.2 ROUTINE CLASSIFICATION TESTS.

Tests for the determination of natural moisture content, bulk density, Atterberg's limit, grain size distribution and specific gravity were performed as per IS code on representative disturbed soil samples, wherever felt necessary. The results were used in classifying the soils of different strata as per IS code 1498-1970.

5.0 PRESENTATION OF TEST RESULT

Results were presented in table form on the following pages.

6.0 METHOD FOR CALCLATION OF ALLOWABLE BEARING CAPACITY

6.1 COHESIVE SOIL

Net ultimate bearing capacity was calculated as per IS-6403-1981.
$qd = cNcScDcIc$

qd = net ultimate bearing capacity

Nc=5.14

Sc=1 for strip footing

Dc=1+0.2*D/B

Ic=1 for vertical loading

c= cohesion obtained through unconfined compression test for depth of 2B/3 below the foundation.

Settlement criteria

$S=H/(1+eo)*Cc*\log((po+p1)/po)$

S= settlement

H=thickness of compressible layer

eo=initial void ratio

po=initial effective pressure

p1=pressure increment

Cc=compression index

6.2 Soil with the value of c &θ

Net ultimate bearing capacity was calculated as per IS 6403-1981

$Qd=cNcScDcIc+q(Nq-1)SqDqIq+0.5R*BNr*Sr*Dr*Ir*w'$

For local shear failure

$\text{Tan } \underline{\theta} = 0.67*\text{Tan}\underline{\theta}$

$C'=2*c/3$

Sc=Sq=Sr=1 for strip footing

$Dc=1+0.2*(D/B)*\text{Tan}(45+\underline{\theta}/2)$

Ic=Iq=Ir=1 for vertical loading

$Dq=Dr=1+0.1*(D/B)\text{Tan}(45+\underline{\theta}/2)$

q=(R-Rw)*D

M= moisture content

R= bulk density of soil

Rw=unit weight of water

L.L.= liquid limit

P.L.=plastic limit

S.L.= shrinkage limit

D=depth below ground level

Settlement criteria

The net allowable bearing capacity for a permissible settlement of 25mm, was obtained by

teng's formula

Qna=3.5*(N-3)*{(B+0.3)/2*B}*{(B+0.3)/2*B}*w'*Fd

N= corrected N

Fd=1+D/B less than or equal to 2

7.0 METHOD FOR CALCLATION OF CAPACITY OF CAST-IN-SITU PLANE PILE AS PER BIS 2911 Part I/Sec 2-1979

7.1 COHESIVE SOIL

Net ultimate bearing capacity of pile is given by :

Q=Ap*Nc*Cp +a * C* As

Ap=cross sectional area of pile toe in cm2

Nc=Bearing capacity factor usually taken as 9

Cp=average cohesion at pile tip in Kg/cm

a=reduction factor

C= average cohesion throughout the length of pile in kg/cm2

As= surface area of pile shaft in cm2

8.0 METHOD FOR CALCLATION OF CAPACITY OF CAST-IN-SITU PLANE PILE AS PER BIS 2911 Part III-1980

8.1 COHESIVE SOIL

Net ultimate bearing capacity of pile is given by :

Q=Ap*Nc*Cp +Aa Nc* C'a + C'a*As'+α*Ca*As

Ap=cross sectional area of pile toe in cm2

Nc=Bearing capacity factor usually taken as 9

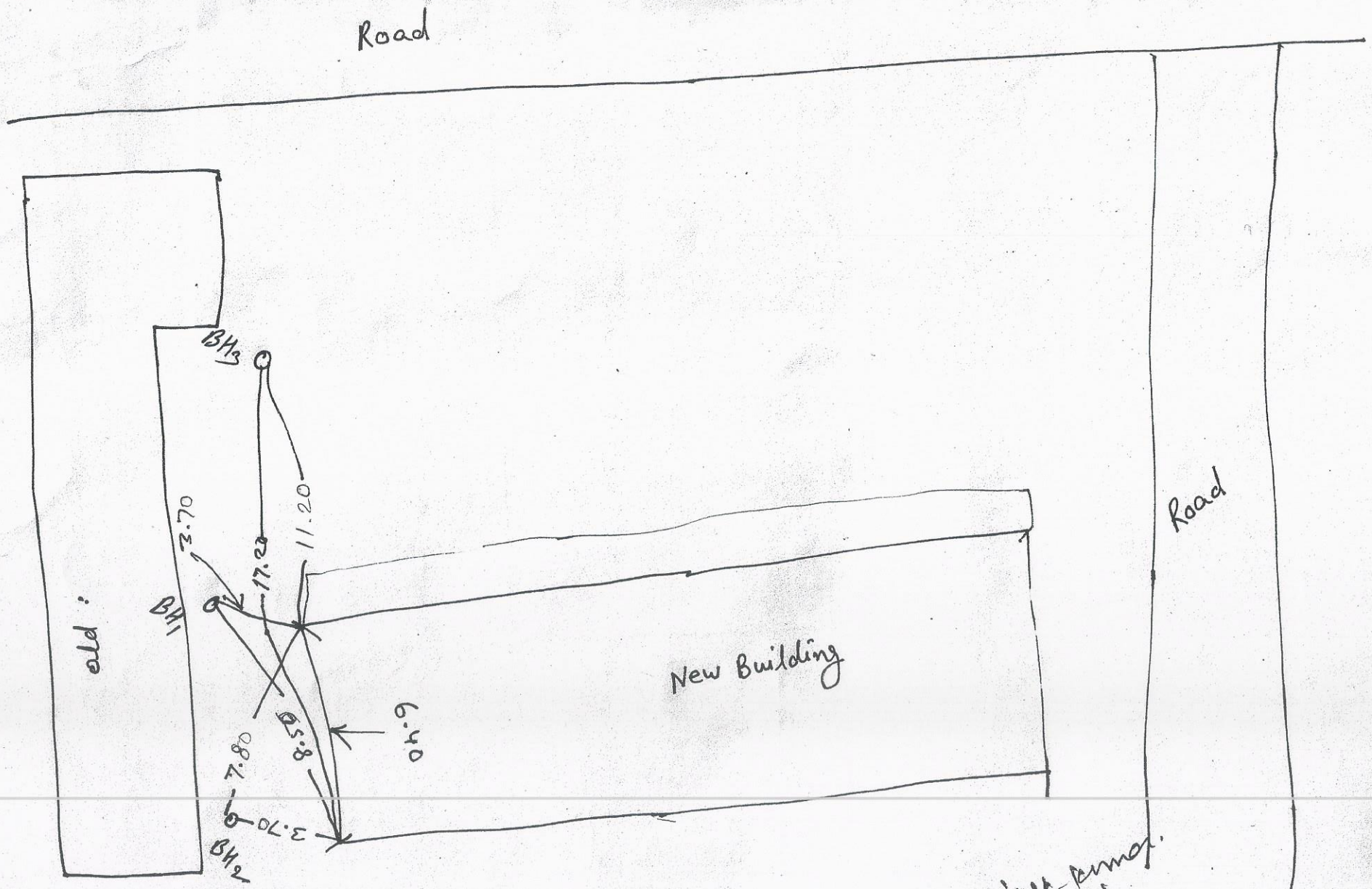
Cp= cohesion of soil around toe.

α=reduction factor

Aa=π*(Du² - D²)/4

C'a= average cohesion around under ream
Du=dia of under-ream,D=dia of pile
As= surface area of pile shaft in cm2
As=surface area of stem
A's=surface area of the cylinder circumscribing the under ream.

Uchch Maadhyamik Vidyalay, Gannipur, Sakraicha, Phulwari, Sarif Patna



SHAMVWI CONSULTANTS ,414J.T.C.,FRASER ROAD, PATNA	NAME OF PROJECT : SOIL INVESTIGATION FOR CONSTRUCTION OF + 2 SCHOOL AT UPGRADED UCCCH MAADHYAMIK VIDYALAY,GANNIPUR,SAKRAICHA,PHULWARI SHARIF,PATNA	BORING DATES	TERMINATION DEPTH :10.5	TABLE NO :2
		START :17.03.2012	WATER TABLE DEPTH . 2.6m	BORE HOLE NO :BH1
		FINISH :17.03.2021		

SAMPLE NO	DEPTH OF SAMPLE	SPT BLOWS PER 30 CM		STANDARD PENETRATION RESISTANCE CURVE	VISUAL DESCRIPTION OF SOIL WITH B.I.S. CLASSIFICATION	GRAIN SIZE ANALYSIS				ATTERBERG'S LIMITS			DENSITY		NATURAL MOISTURE CONTENT (%)	SPECIFIC GRAVITY	SHEAR TEST			CONSISTENCY LIMITS		UNCONFINED COMPRESSION TEST ,q kg/cm2	COEFFICIENT OF VOLUME COMPRESSIBILITY Mv cm3/kg
		OBSERVED VALUE	CORRECTED VALUE	5 10 20			SAND (%)	SILT (%)	CLAY (%)	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX	BULK DENSITY (gm/cm3)	DRY DENSITY(gm/cm3)			TYPE OF TEST	COHESION c (kg/cm2)	ANGLE OF FRICTION IN DEGREE	VOID RATIO eo	COMPRESSION INDEX Cc		
DS	G.L.																						
UDS 1					Blackish Clay CI																		
SPT1	1.5	20				0.0	2.70	97.3		38	18	20	2.01	1.70	18.2	2.61	UUT	0.4	18.0	0.76	0.10		
UDS 2					Silty Clay CI																		
SPT2	3	25				0.0	3.80	96.2		42	22	20	2.01	1.68	19.9	2.62							
UDS 3					Silty Clay CI																		
SPT3	4.5	26				0.0	1.50	98.5		42	22	20	2.01	1.67	20.5	2.62	UUT	0.5	20.00				
UDS 4					Reddish Silty Clay CI																		
SPT4	6	27				0.4	1.40	98.2		42	22	20	2.01	1.63	23.1	2.62							

UUT : UNCONSOLIDATED UNDRAINED TRIAXIAL SHEAR TEST

UCT : UNCONFINED COMPRESSION SHEAR TEST

DST : DIRECT SHEAR TEST

! SAMPLE SLIPED ~ TEST ON REMOULDED SAMPLE

UDS : UNDISTURBED SAMPLE

SPT : STANDARD PENETRATION TEST VALUE

NOTES : CONSOLIDATION TEST RESULTS ARE FOR THE LOADING RANGE OF 5.0-10.0 t/m2

SHAMVWI CONSULTANTS ,414J.T.C.,FRASER ROAD, PATNA	NAME OF PROJECT : SOIL INVESTIGATION FOR CONSTRUCTION OF + 2 SCHOOL AT UPGRADED UCCCH MAADHYAMIK VIDYALAY,GANNIPUR,SAKRAICHA,PHULWARI SHARIF,PATNA	BORING DATES	TERMINATION DEPTH :10.5	TABLE NO :3
		START :17.03.2012	WATER TABLE DEPTH : 2.6m	BORE HOLE NO :BH1
		FINISH :17.03.2021		

SAMPLE NO	DEPTH OF SAMPLE	SPT BLOWS PER 30 CM		STANDARD PENETRATION RESISTANCE CURVE	VISUAL DESCRIPTION OF SOIL WITH B.I.S. CLASSIFICATION	GRAIN SIZE ANALYSIS				ATTERBERG'S LIMITS			DENSITY		NATURAL MOISTURE CONTENT (%)	SPECIFIC GRAVITY	SHEAR TEST			CONSISTENCY LIMITS		UNCONFINED COMPRESSION TEST ,q kg/cm2	COEFFICIENT OF VOLUME COMPRESSIBILITY Mv cm3/kg
		OBSERVED VALUE	CORRECTED VALUE	5 10 20		GRAVEL (%)	SAND (%)	SILT (%)	CLAY (%)	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX	BULK DENSITY (gm/cm3)	DRY DENSITY(gm/cm3)			TYPE OF TEST	COHESION c (kg/cm2)	ANGLE OF FRICTION IN DEGREE	VOID RATIO eo	COMPRESSION INDEX Cc		
UDS 5					Reddish Silty Clay CI																		
SPT5	7.5	18				0.0	0.90	99.1		41	23	18	2.01	1.62	23.8	2.63	UUT	0.5	12.00				
UDS 6					Reddish Silty Clay CI																		
SPT6	9.0	20				0.5	4.40	95.1		41	23	18	2.01	1.62	23.8	2.65							
UDS 7					Reddish Silty Clay CI																		
SPT7	10.5	17				0.4	1.40	98.2		41	23	18	2.01	1.61	24.5	2.65	UUT	0.5	12.00				

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		START :17.03.2012	WATER TABLE DEPTH : 2.6m	BORE HOLE NO :BH2
		FINISH :18.03.2021		

SAMPLE NO	DEPTH OF SAMPLE	SPT BLOWS PER 30 CM		STANDARD PENETRATION RESISTANCE CURVE	VISUAL DESCRIPTION OF SOIL WITH B.I.S. CLASSIFICATION	GRAIN SIZE ANALYSIS				ATTERBERG'S LIMITS			DENSITY		NATURAL MOISTURE CONTENT (%)	SPECIFIC GRAVITY	SHEAR TEST			CONSISTENCY LIMITS		UNCONFINED COMPRESSION TEST ,q kg/cm2	COEFFICIENT OF VOLUME COMPRESSIBILITY Mv cm3/kg
		OBSERVED VALUE	CORRECTED VALUE	5 10 20			SAND (%)	SILT (%)	CLAY (%)	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX	BULK DENSITY (gm/cm3)	DRY DENSITY(gm/cm3)			TYPE OF TEST	COHESION c (kg/cm2)	ANGLE OF FRICTION IN DEGREE	VOID RATIO eo	COMPRESSION INDEX Cc		
DS	G.L.																						
UDS 1					Blackish Clay CI																		
SPT1	1.5	19				0.1	2.90	97.0		38	18	20	2.01	1.69	19.2	2.61	UUT	0.4	18.0				
UDS 2					Silty Clay CI																		
SPT2	3	23				0.1	3.90	96.0		42	22	20	2.01	1.68	19.6	2.62							
UDS 3					Silty Clay CI																		
SPT3	4.5	24				0.5	1.70	97.8		42	22	20	2.01	1.67	20.4	2.62	UUT	0.5	20.00				
UDS 4					Reddish Silty Clay CI																		
SPT4	6	26				0.5	1.43	98.1		42	22	20	2.01	1.64	22.8	2.62							

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		START :17.03.2012	WATER TABLE DEPTH : 2.6m	BORE HOLE NO :BH2
		FINISH :18.03.2021		

SAMPLE NO	DEPTH OF SAMPLE	SPT BLOWS PER 30 CM		STANDARD PENETRATION RESISTANCE CURVE	VISUAL DESCRIPTION OF SOIL WITH B.I.S. CLASSIFICATION	GRAIN SIZE ANALYSIS				ATTERBERG'S LIMITS			DENSITY		NATURAL MOISTURE CONTENT (%)	SPECIFIC GRAVITY	SHEAR TEST			CONSISTENCY LIMITS		UNCONFINED COMPRESSION TEST ,q kg/cm2	COEFFICIENT OF VOLUME COMPRESSIBILITY Mv cm3/kg
		OBSERVED VALUE	CORRECTED VALUE	5 10 20		GRAVEL (%)	SAND (%)	SILT (%)	CLAY (%)	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX	BULK DENSITY (gm/cm3)	DRY DENSITY(gm/cm3)			TYPE OF TEST	COHESION c (kg/cm2)	ANGLE OF FRICTION IN DEGREE	VOID RATIO eo	COMPRESSION INDEX Cc		
UDS 5					Reddish Silty Clay CI																		
SPT5	7.5	17				0.0	1.20	98.8		41	23	18	2.01	1.63	23.3	2.63	UUT	0.5	12.00				
UDS 6					Reddish Silty Clay CI																		
SPT6	9.0	22				0.6	4.20	95.2		41	23	18	2.01	1.63	23.6	2.65							
UDS 7					Reddish Silty Clay CI																		
SPT7	10.5	22				0.6	1.45	98.0		41	23	18	2.01	1.62	23.8	2.65	UUT	0.5	12.00				

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		START :17.03.2012	WATER TABLE DEPTH : 2.6m	BORE HOLE NO :BH3
		FINISH :18.03.2021		

SAMPLE NO	DEPTH OF SAMPLE	SPT BLOWS PER 30 CM		STANDARD PENETRATION RESISTANCE CURVE	VISUAL DESCRIPTION OF SOIL WITH B.I.S. CLASSIFICATION	GRAIN SIZE ANALYSIS				ATTERBERG'S LIMITS			DENSITY		NATURAL MOISTURE CONTENT (%)	SPECIFIC GRAVITY	SHEAR TEST			CONSISTENCY LIMITS		UNCONFINED COMPRESSION TEST ,q kg/cm2	COEFFICIENT OF VOLUME COMPRESSIBILITY Mv cm3/kg
		OBSERVED VALUE	CORRECTED VALUE	5 10 20			SAND (%)	SILT (%)	CLAY (%)	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX	BULK DENSITY (gm/cm3)	DRY DENSITY(gm/cm3)			TYPE OF TEST	COHESION c (kg/cm2)	ANGLE OF FRICTION IN DEGREE	VOID RATIO eo	COMPRESSION INDEX Cc		
DS	G.L.																						
UDS 1					Blackish Clay CI																		
SPT1	1.5	18				0.1	2.60	97.3		38	18	20	2.01	1.68	19.8	2.61	UUT	0.4	18.0				
UDS 2					Silty Clay CI																		
SPT2	3	26				0.1	4.10	95.8		42	22	20	2.01	1.67	20.1	2.62							
UDS 3					Silty Clay CI																		
SPT3	4.5	27				0.6	1.60	97.8		42	22	20	2.01	1.67	20.6	2.62	UUT	0.5	20.00				
UDS 4					Reddish Silty Clay CI																		
SPT4	6	26				0.5	1.70	97.8		42	22	20	2.01	1.63	23.6	2.62							

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		START :17.03.2012	WATER TABLE DEPTH : 2.6m	BORE HOLE NO :BH3
		FINISH :18.03.2021		

SAMPLE NO	DEPTH OF SAMPLE	SPT BLOWS PER 30 CM		STANDARD PENETRATION RESISTANCE CURVE	VISUAL DESCRIPTION OF SOIL WITH B.I.S. CLASSIFICATION	GRAIN SIZE ANALYSIS				ATTERBERG'S LIMITS			DENSITY		NATURAL MOISTURE CONTENT (%)	SPECIFIC GRAVITY	SHEAR TEST			CONSISTENCY LIMITS		UNCONFINED COMPRESSION TEST ,q kg/cm2	COEFFICIENT OF VOLUME COMPRESSIBILITY Mv cm3/kg
		OBSERVED VALUE	CORRECTED VALUE	5 10 20		GRAVEL (%)	SAND (%)	SILT (%)	CLAY (%)	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX	BULK DENSITY (gm/cm3)	DRY DENSITY(gm/cm3)			TYPE OF TEST	COHESION c (kg/cm2)	ANGLE OF FRICTION IN DEGREE	VOID RATIO eo	COMPRESSION INDEX Cc		
UDS 5					Reddish Silty Clay CI																		
SPT5	7.5	20				0.0	1.30	98.7		41	23	18	2.01	1.64	22.9	2.63	UUT	0.5	12.00				
UDS 6					Reddish Silty Clay CI																		
SPT6	9.0	20				0.6	4.10	95.3		41	23	18	2.01	1.63	23.6	2.65							
UDS 7					Reddish Silty Clay CI																		
SPT7	10.5	17				0.6	1.60	97.8		41	23	18	2.01	1.63	23.6	2.65	UUT	0.5	12.00				

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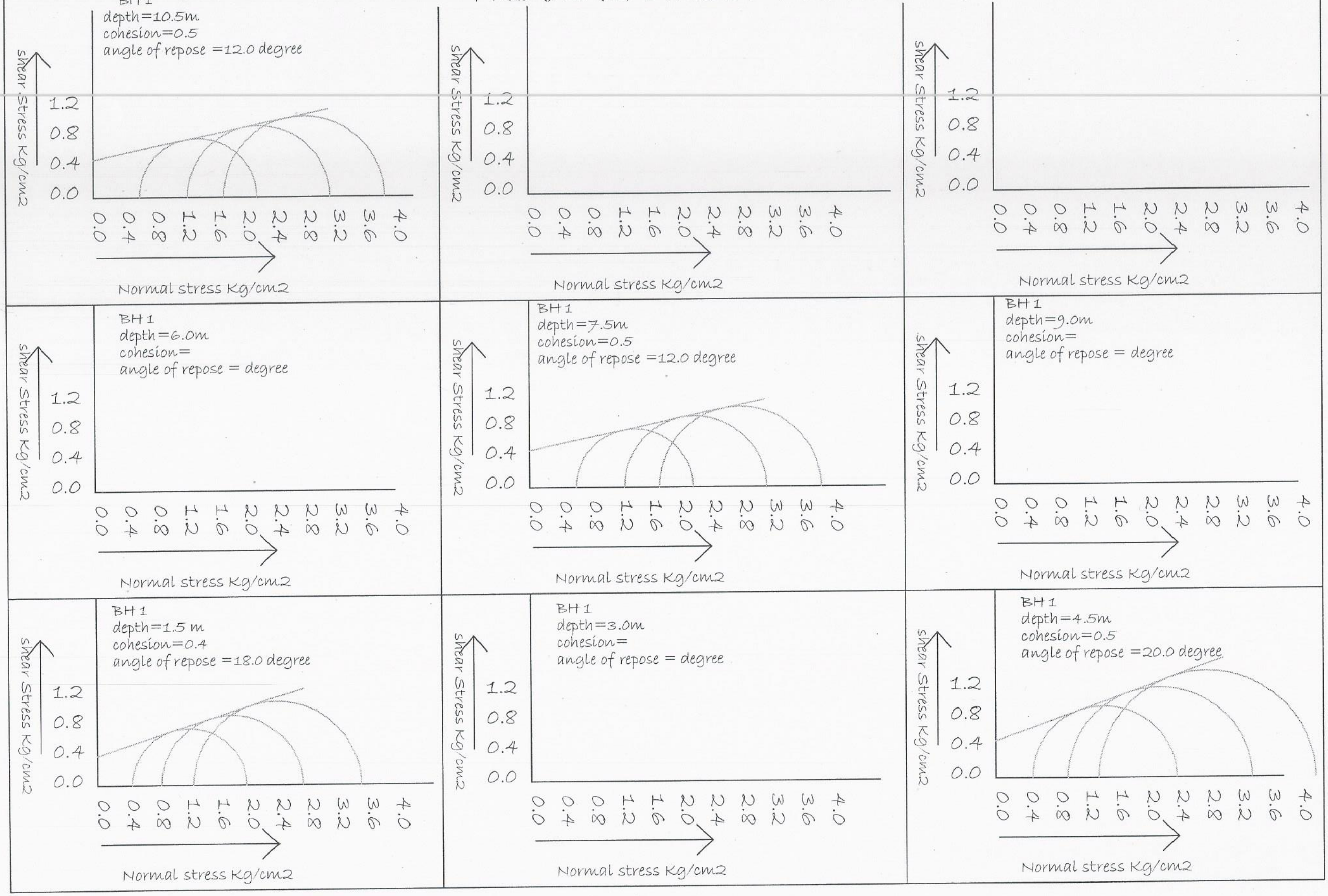
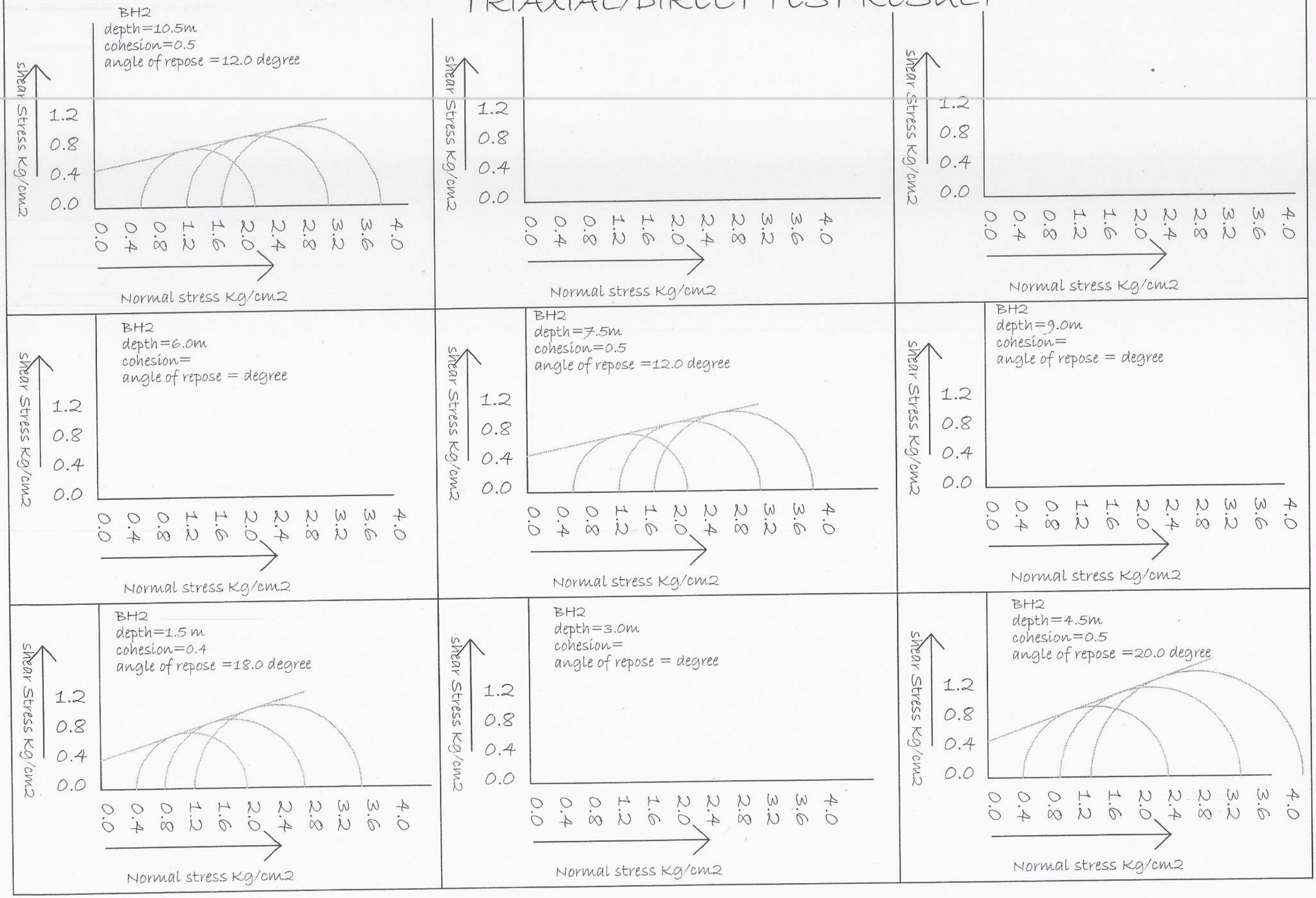
2 SCHOOL AT UPGRADED UCCCH MAADHYAMIK VIDYALAY,GANNIPUR,SAKRAICHA,PHULWARI SHARIF,PATI

TRIAXIAL/DIRECT TEST RESULT

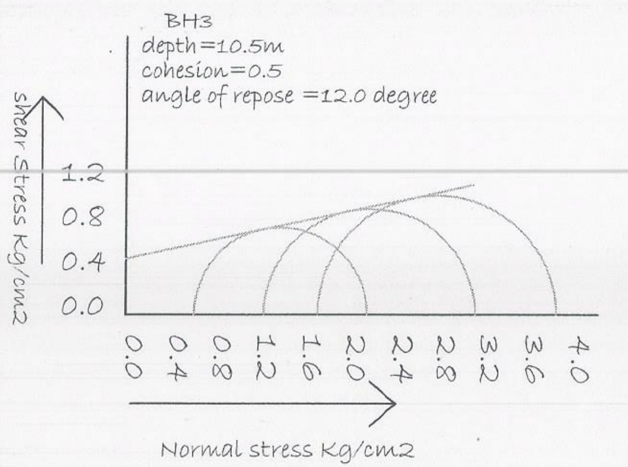


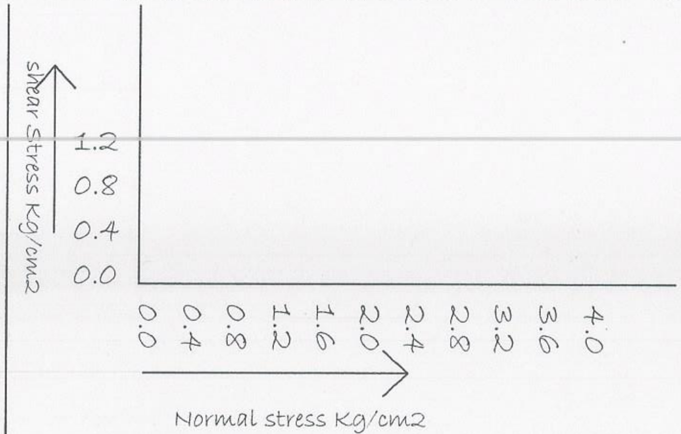
TRIAXIAL/DIRECT TEST RESULT

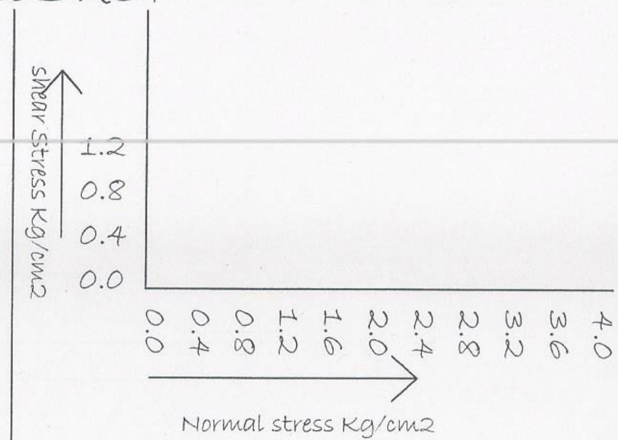


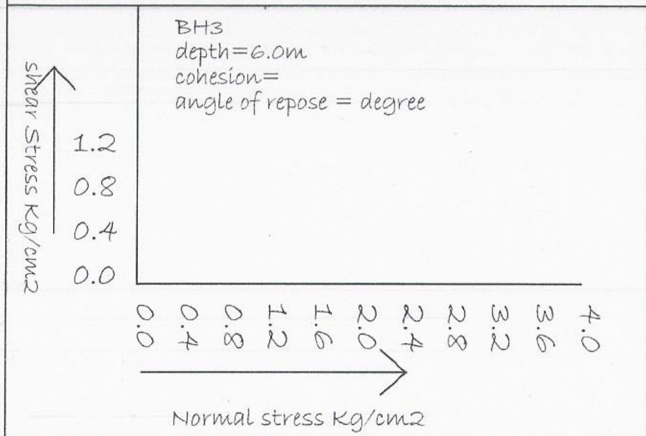
2 SCHOOL AT UPGRADED UCCCH MAADHYAMIK VIDYALAY,GANNIPUR,SAKRAICHA,PHULWARI SHARIF,PATI

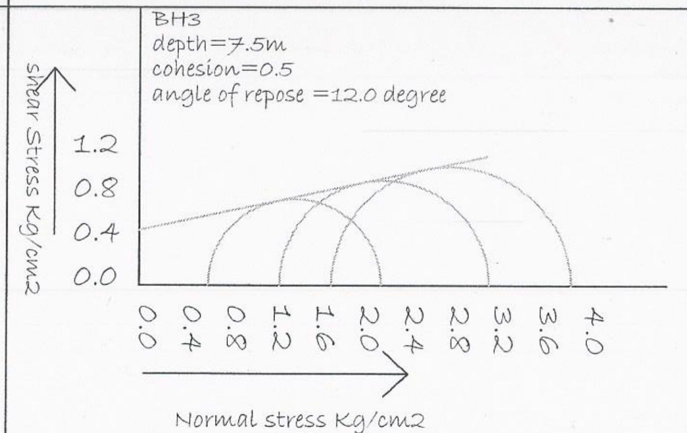
TRIAXIAL/DIRECT TEST RESULT

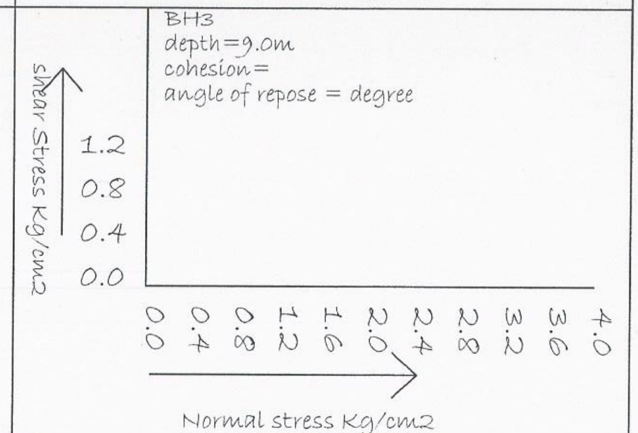


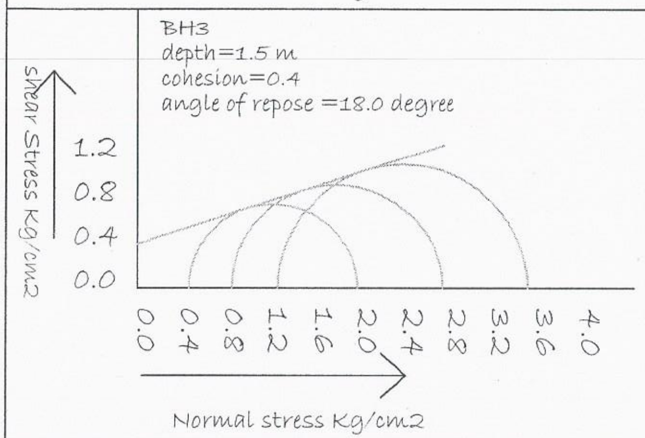


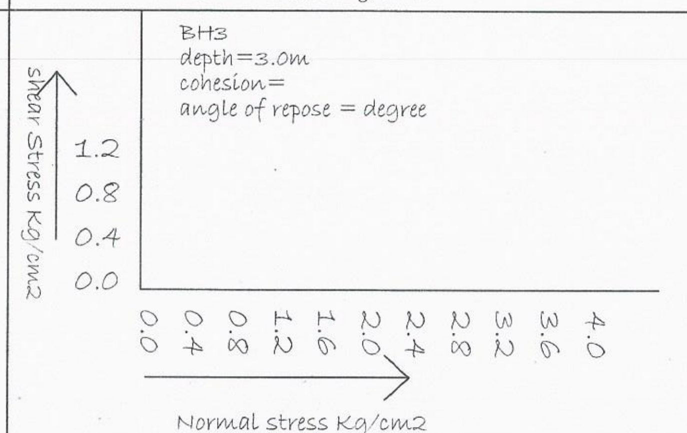


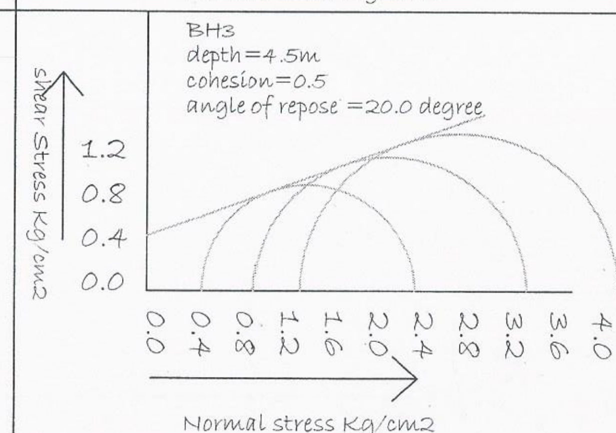




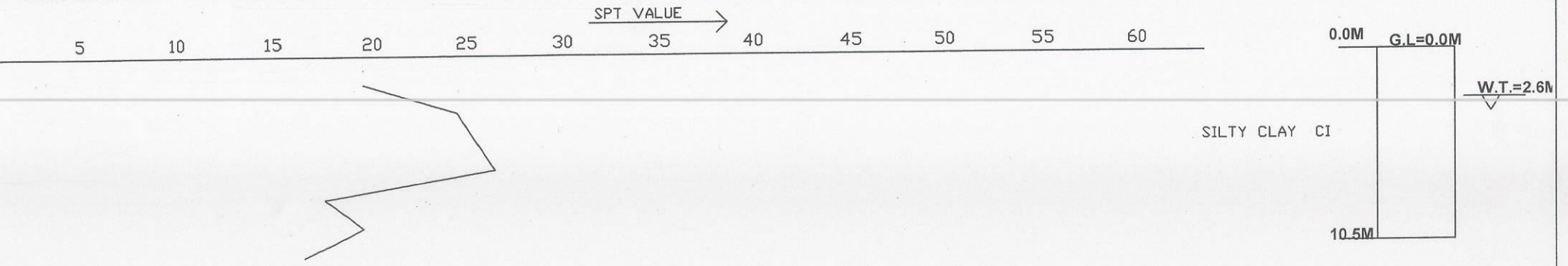








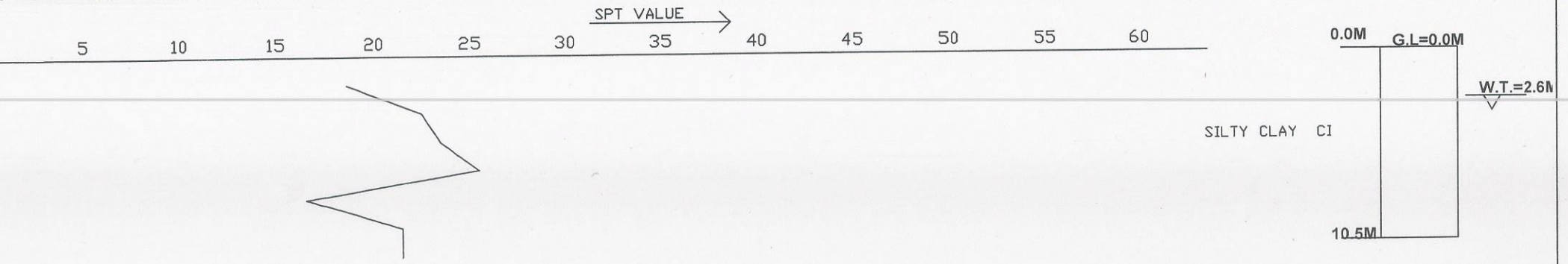
LOG AND DEPTH ~ SPT GRAPH (+ 2 SCHOOL AT UPGRADED UCCCH MAADHYAMIK VIDYALAY,GANNIPUR,SAKRAICHA,PHULWARI SHARIF,PA



BORE LOG

BH1

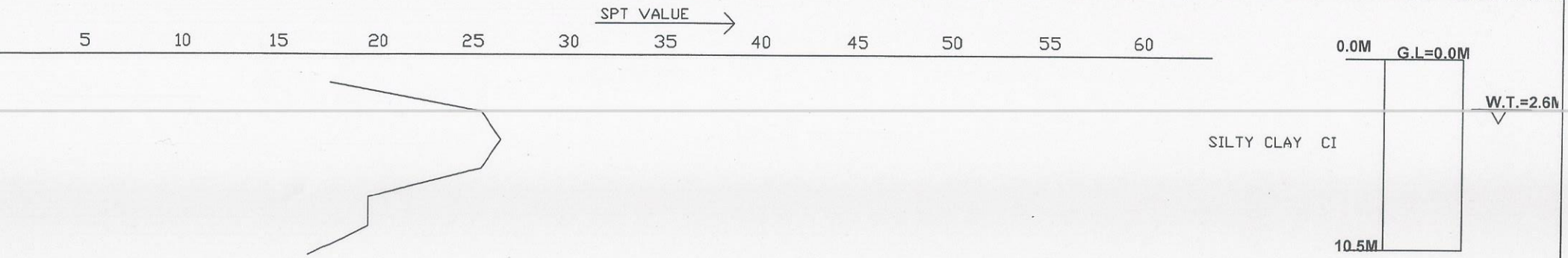
E LOG AND DEPTH ~ SPT GRAPH (+ 2 SCHOOL AT UPGRADED UCCCH MAADHYAMIK VIDYALAY,GANNIPUR,SAKRAICHA,PHULWARI SHARIF,PA



BORE LOG

BH2

E LOG AND DEPTH ~ SPT GRAPH (+ 2 SCHOOL AT UPGRADED UCCCH MAADHYAMIK VIDYALAY,GANNIPUR,SAKRAICHA,PHULWARI SHARIF,PA

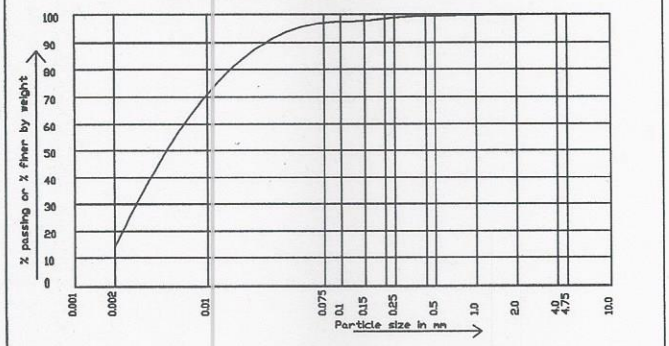


BORE LOG

BH3

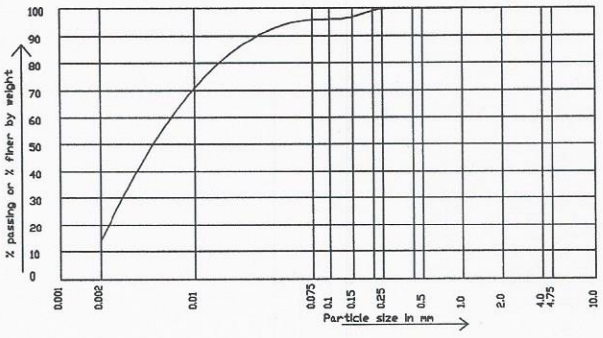
+ 2 SCHOOL AT UPGRADED UCCCH MAADHYAMIK VIDYALAY,GANNIPUR,SAKRAICHA,PHULWARI SHARIF,PATNA

GRAIN SIZE DISTRIBUTION CURVE (BH1 & DEPTH =1.5m)



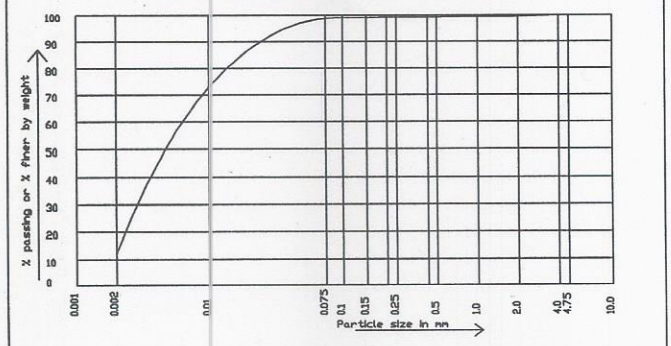
+ 2 SCHOOL AT UPGRADED UCCCH MAADHYAMIK VIDYALAY,GANNIPUR,SAKRAICHA,PHULWARI SHARIF,PATNA

GRAIN SIZE DISTRIBUTION CURVE (BH1 & DEPTH =3.0m)



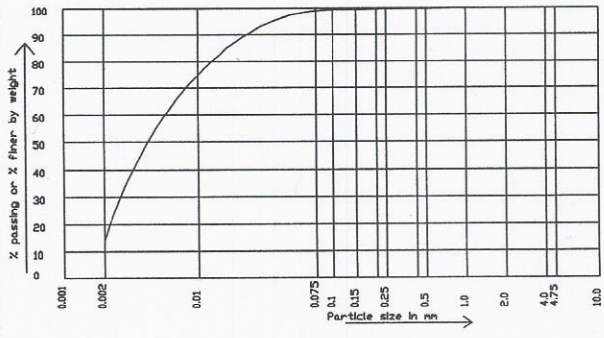
+ 2 SCHOOL AT UPGRADED UCCCH MAADHYAMIK VIDYALAY,GANNIPUR,SAKRAICHA,PHULWARI SHARIF,PATNA

GRAIN SIZE DISTRIBUTION CURVE (BH1 & DEPTH =4.5m)



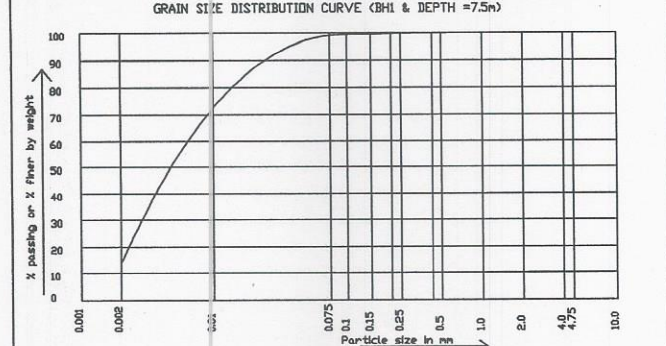
+ 2 SCHOOL AT UPGRADED UCCCH MAADHYAMIK VIDYALAY,GANNIPUR,SAKRAICHA,PHULWARI SHARIF,PATNA

GRAIN SIZE DISTRIBUTION CURVE (BH1 & DEPTH =6.0m)



+ 2 SCHOOL AT UPGRADED UCCCH MAADHYAMIK VIDYALAY,GANNIPUR,SAKRAICHA,PHULWARI SHARIF,PATNA

GRAIN SIZE DISTRIBUTION CURVE (BH1 & DEPTH =7.5m)



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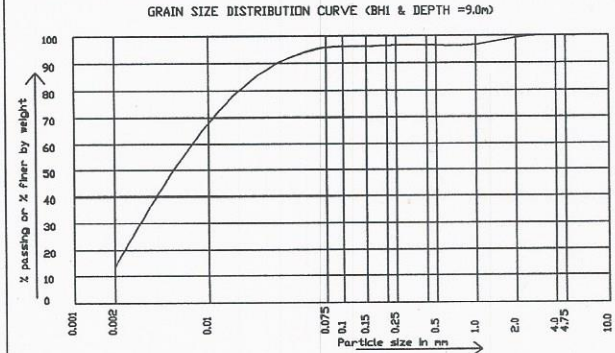
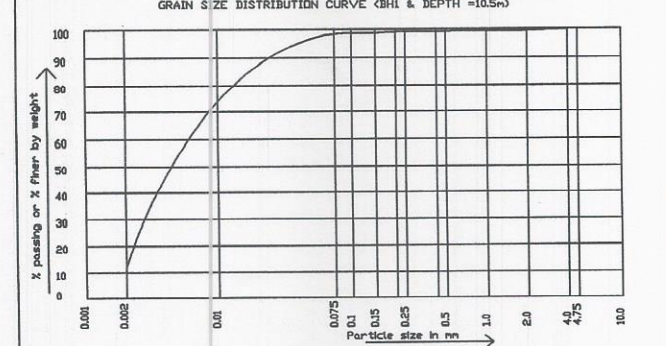
GRAIN SIZE DISTRIBUTION CURVE (BH1 & DEPTH =9.0m)



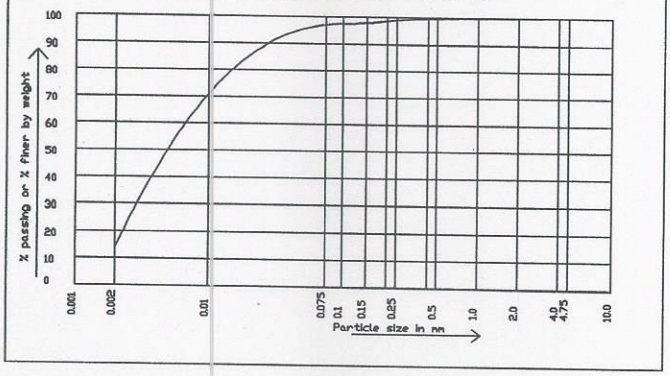
+ 2 SCHOOL AT UPGRADED UCCCH MAADHYAMIK VIDYALAY,GANNIPUR,SAKRAICHA,PHULWARI SHARIF,PATNA

GRAIN SIZE DISTRIBUTION CURVE (BH1 & DEPTH =10.5m)



+ 2 SCHOOL AT UPGRADED UCCCH MAADHYAMIK VIDYALAY,GANNIPUR,SAKRAICHA,PHULWARI SHARIF,PATNA

GRAIN SIZE DISTRIBUTION CURVE (BH2 & DEPTH =1.5m)



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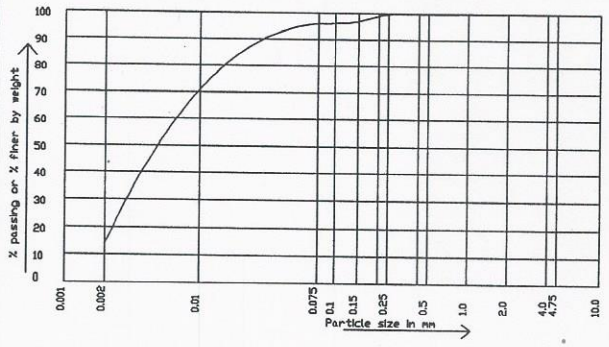
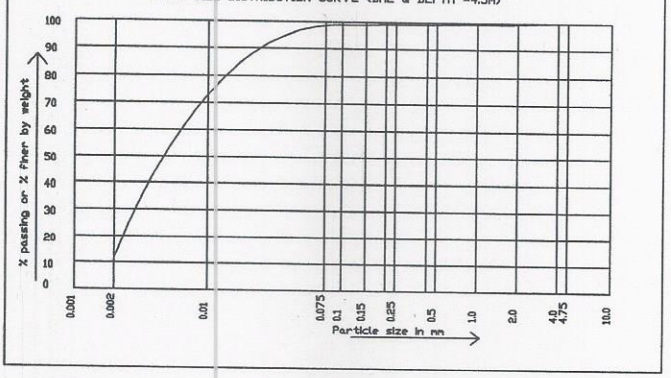
GRAIN SIZE DISTRIBUTION CURVE (BH2 & DEPTH =3.0m)



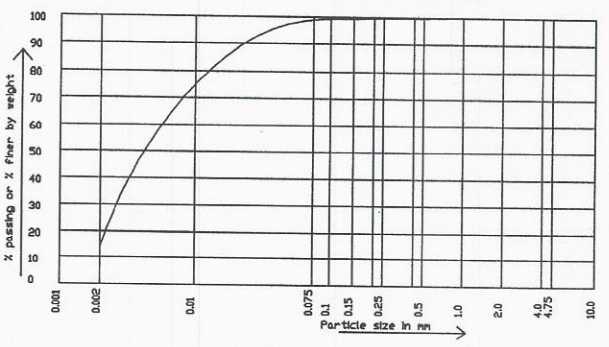
+ 2 SCHOOL AT UPGRADED UCCCH MAADHYAMIK VIDYALAY,GANNIPUR,SAKRAICHA,PHULWARI SHARIF,PATNA

GRAIN SIZE DISTRIBUTION CURVE (BH2 & DEPTH =4.5m)



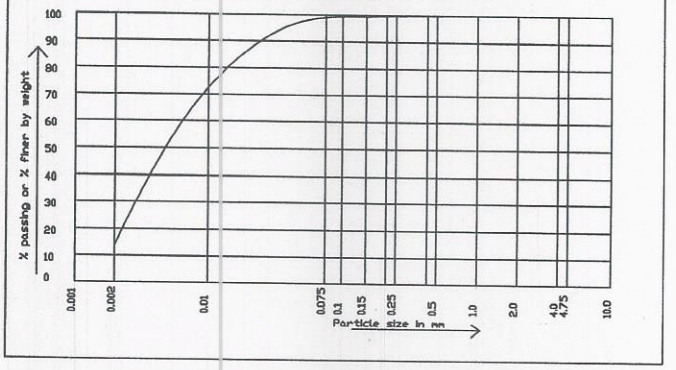
+ 2 SCHOOL AT UPGRADED UCCCH MAADHYAMIK VIDYALAY,GANNIPUR,SAKRAICHA,PHULWARI SHARIF,PATNA

GRAIN SIZE DISTRIBUTION CURVE (BH2 & DEPTH =6.0m)



+ 2 SCHOOL AT UPGRADED UCCCH MAADHYAMIK VIDYALAY,GANNIPUR,SAKRAICHA,PHULWARI SHARIF,PATNA

GRAIN SIZE DISTRIBUTION CURVE (BH2 & DEPTH =7.5m)



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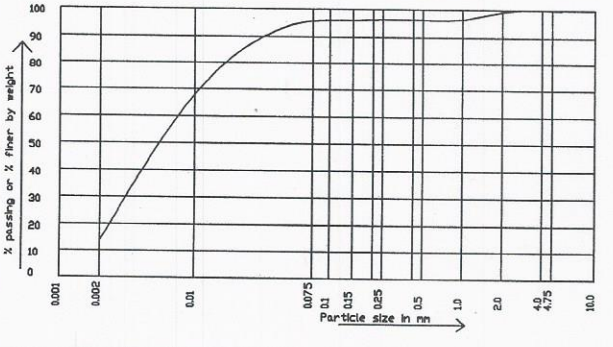
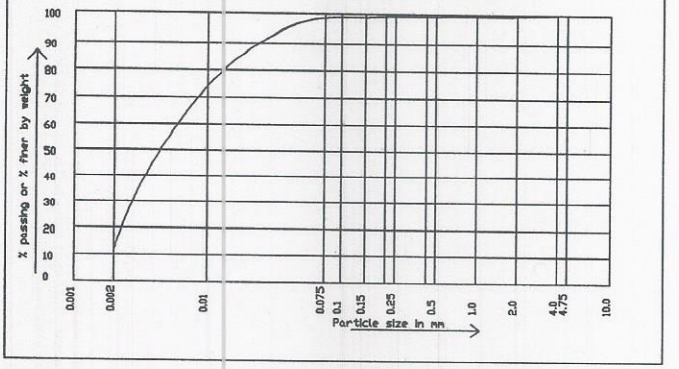
GRAIN SIZE DISTRIBUTION CURVE (BH2 & DEPTH =9.0m)



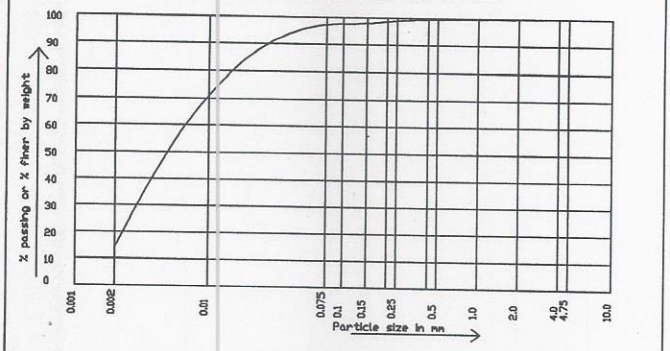
+ 2 SCHOOL AT UPGRADED UCCCH MAADHYAMIK VIDYALAY,GANNIPUR,SAKRAICHA,PHULWARI SHARIF,PATNA

GRAIN SIZE DISTRIBUTION CURVE (BH2 & DEPTH =10.5m)



+ 2 SCHOOL AT UPGRADED UCCCH MAADHYAMIK VIDYALAY,GANNIPUR,SAKRAICHA,PHULWARI SHARIF,PATNA

GRAIN SIZE DISTRIBUTION CURVE (BH3 & DEPTH =1.5m)



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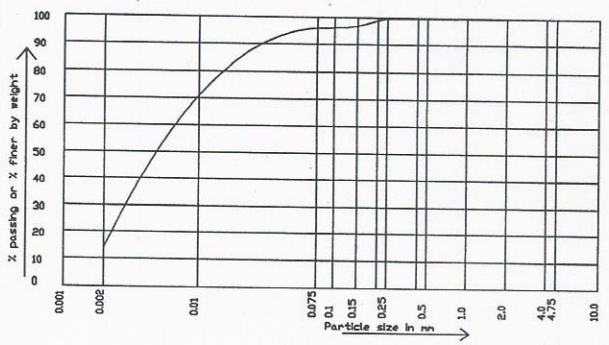
GRAIN SIZE DISTRIBUTION CURVE (BH3 & DEPTH =3.0m)



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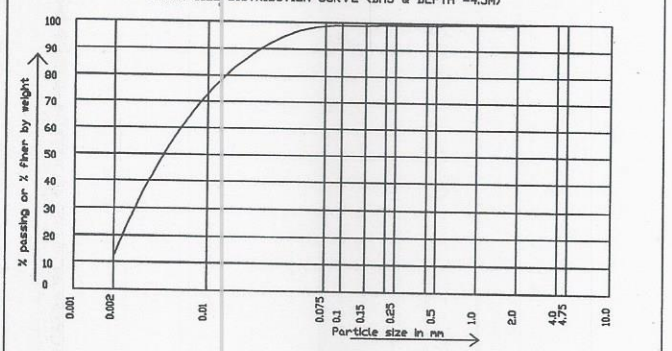
GRAIN SIZE DISTRIBUTION CURVE (BH3 & DEPTH =4.5m)



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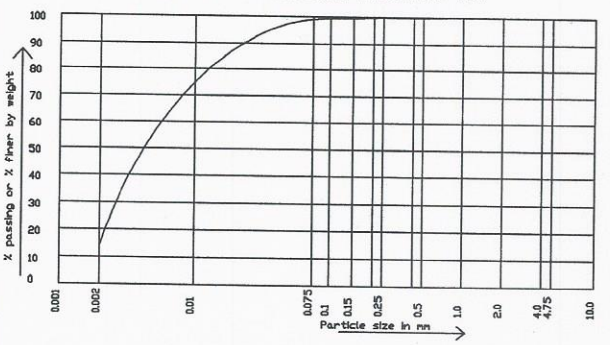
GRAIN SIZE DISTRIBUTION CURVE (BH3 & DEPTH =6.0m)



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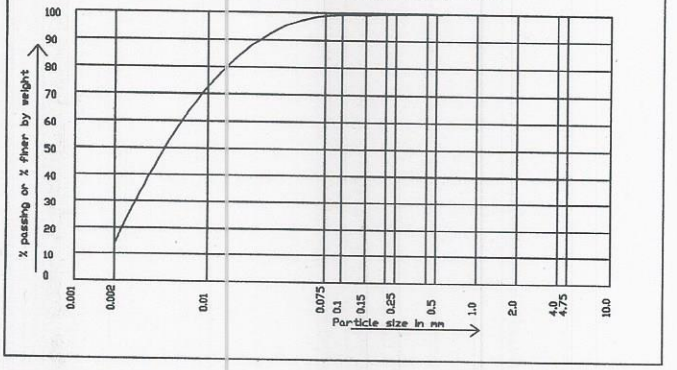
GRAIN SIZE DISTRIBUTION CURVE (BH3 & DEPTH =7.5m)



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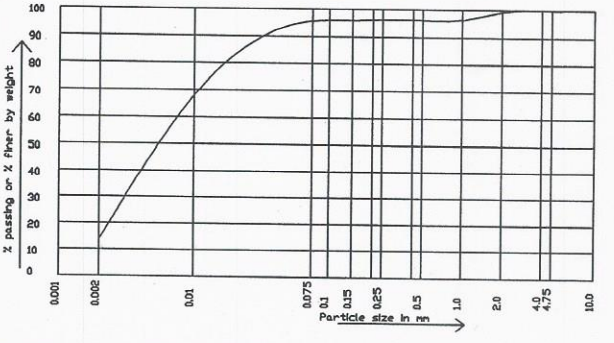
GRAIN SIZE DISTRIBUTION CURVE (BH3 & DEPTH =9.0m)



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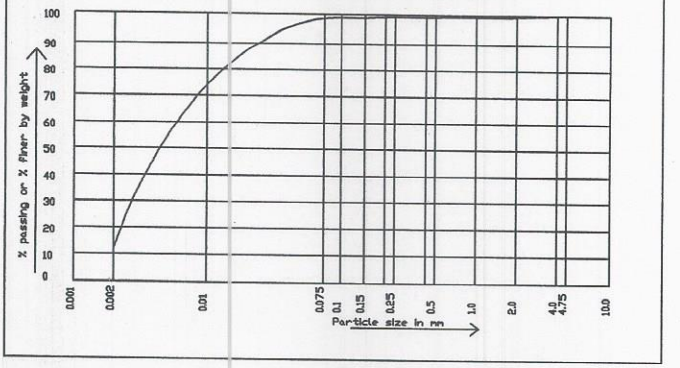
GRAIN SIZE DISTRIBUTION CURVE (BH3 & DEPTH =10.5m)



NAME OF PROJECT : SOIL INVESTIGATION FOR CONSTRUCTION OF + 2 SCHOOL AT UPGRADED UCCCH MAADHYAMIK VIDYALAY,GANNIPUR,SAKRAICHA,PHULWARI SHARIF,PATNA

Calculation of settelement in clay for Footing as per IS : 8009 (Part I)-1976

Width,B of FOOTING in meter	2.00	The seat of settlement is assumed as zone bounded by the 20% vertical stress contour.								
		=σz /p =								0.2
bearing capacity of soil in ton /m2 =	7	Where σz /q =			0.2					
Unit weight of soil in ton/m2 =	2.01	L=		2	m	B=	2.00	m	Area=	4
Height of compressible soil in meter =H	9.00	Foundation area Equivalent to circular area,for simplicity=="pi()*D^2/4="							4	m2
initial void ratio e0=	0.76	Dia of Equivalent Circular area=2R=					2.257	m		
Compression index Cc=	0.10	R=			1.13	m				
Depth of Foundation in meter=	1.5	Using Boussinesq's expression for vertical stress below NGL,Cl B-1.3 of IS 8009(Part1),we get following								
Length of Footing=	2	m								
		$\sigma_z /p = [1-\{1/(1+(R/z)^2)\}^{3/2}]$ =								
		consider z=			9	m	trial			
R/z=	0.126	σ_z /p=		0.02	not ok		0.2			
		z=Height of compresible strata=					9.00	m		
NGL=0.0M										
Bot of Footing Lv=	1.5	Top of Basement Lv=			1.1	m	below internal Road			
		Bot of Footing Lv=			1.5	m	below internal Road			
Effective height for Initial Stress=1.5-1.1=	0.4									

Backfiling /Concreting is done for thickness over foundation Lv=1.5-1.1=0.4m. so initial effective stress is calculated on this depth.

Determination of Bearing pressure at different depth below footing level factor for footing

Initial Effective stress at the top of clay layer=po=1.5x(0.4-1)=		0.404	t/m2	
Initial Effective stress at the bottom of clay layer=po=0.404+9x(2.01-1)=		9.494	t/m2	
Average Effective stress on the clay stratum before construction=(0.404+9.494)/2=				
	=	4.95	t/m2	p0
Additional Stress at the top of stratum due to construction=		7	t/m2	
Additional Stress at the bottom of stratum due to construction=7x2/(9+2)=		1.27	t/m2	
Average increase in stress after construction=(7+1.27)/2=	4.135		t/m2	
Hence Average effective stress on the clay stratum after construction=4.95+4.135=				
	=	9.1	t/m2	(p0+p1)
Settelement s in mm =s=H/(1+e0)*Cc*Log10((po+p1)/p0)=0.1x9000x(LOG10(9.1/4.95))/(1+0.76)=				
	=	135.2		

D/sqrt(L*B)	0.75	
Final D/sqrt(L*B)=	0.75	
L/B=	1.00	
Correction for Depth Factor=	0.8	from Cl 9.5.1 and Fig12 of IS 8009(Part1)
Correction for normally consolidated soil=	0.7	from Table1 of IS 8009(Part1)
Correction for rigidity=	0.8	from Cl 9.5.2 of IS 8009(Part1)
Corrected Settelement s in mm=135.2x0.8x0.7x0.8=	61	mm

SAMPLE CALCULATION OF CAPACITY OF UNDER REAM PILE for								NAME OF PROJECT : SOIL INVESTIGATION FOR CONSTRUCTION OF + 2 SCHOOL AT UPGRADED UCCCH MAADHYAMIK VIDYALAY,GANNIPUR,SAKRAICHA,PHULWARI SHARIF,PATNA				
The load carrying capacity of the pile has been calculated using IS : 2911 (Part III) 1980,Clause 5.2.3.1												
These calculations are based on												
(a) in fine- grained soils, only on cohesion (c). In t/m², taking angle of internal friction = 0												
This is likely to give the minimum capacity of the pile												
Pile diameter, D (m) =	0.3	Hence, area of pile base. Ap (m²) =		0.071	& circumference (in m) of pile base j =		0.942					
Under ream, diameter, Du (m) =	0.75	Hence, Aa (m²) =	0.37	Spacing between under ream in m =		1.13	Hence, A's (m²) =	2.66				
The following values are taken in view of the codal provisions :							Surface area of pile's contact with soil, As (m²) = j x t					
Reduction factor, α, depending on N.		0.5					where t = thickness of soil layer in contact with pile.					
Skin friction in clay, Qs = α *Ca*As.		Total Ultimate capacity of pile, Qu = Ap*Nc*Cp + Aa*Nc*C'a +C'a*A's										
Total Ultimate capacity of pile, Qu = Ap*Nc*Cp + Aa*Nc*C'a +C'a*A's + Qs						Nc=	9					
Safe capacity of pile, Qsf = Qs / fs1 + Qb / fs1												
takeing factor of safety =		2.5										
Depth of soil layer (m)	Soil type	Average cohesion Ca	cohesion cp t/m²	Thickness of layer, t [m]	Average cohesion C'a	As = m²	Ap*Nc*Cp I	Aa*Nc*C'a II	C'a*A's III	Qs = α *Ca*As IV	Ultimate capacity (TON)	Safe capacity (TON)
8	clay	5	6	8	5	6.47	3.83	16.65	13.30	16.18	49.96	20.0

Table 8

Soil stratification

DEPTH	SOIL TYPE	CONSISTANCY	CLASSIFICATION
0.0-10.5	BLACKISH/ REDDISH SILTY CLAY	MEDIUM	CI

Water table has been reported at 2.5m below NGL as reported in the month of March'2021.

RECOMMENDATION

The present report is prepared on the basis of lab. Test result & field test conducted in the field.

The lab. test result is obtained by conducting different test on representative sample obtained through 3 no. of bore holes whose location and depth were decided by BSEIDC and shown in the bore hole location plan.

The laboratory test of soil samples obtained in all bore holes are given in Tables 2-7. Study of these tables reveals that the sub-soil strata :

(a) Soil strata consist of fine grained soil.

Therefore, foundation should be placed at 1.50m or beyond the ground level. Both, shallow as well as deep, foundations are feasible. Bore Hole may cave in. Therefore, Bentonite slurry or casing is required for the bore hole stabilization.

By way of example the calculated value of safe capacity of certain type and size of Shallow foundation are being tabulated below: -

Shallow foundation

STRIP FOOTING

Depth below GL (m)	Width of foundation (m)	Maximum expected settlement (mm)	Allowable Bearing capacity (t/m2)
1.5	2.0	60	7.0

By way of example the calculated value of safe capacity of certain diameter of under reamed pile using IS : 2911 (Part III) 1980,Clause 5.2.3.1 are being tabulated below: -

Double Under reamed Pile

Depth of Pile below GL(m)	Dia of Pile (m)	Dia of Under ream (m)	Allowable Capacity (Ton)
8.0	0.3	0.75	20
8.0	0.4	1.0	25

Limitation

If the sub-soil condition is found much different from those reported here during trenching, suitable steps should be taken. Back filling over footing shall be done with proper compaction.

Pile capacity shall be confirmed by Initial and Routine pile load test, before starting the work, as per relevant Indian codes.

Subodh Kumar Sinha

SUBODH KUMAR SINHA
Partner Shamvwi consultant